A New Metamodeling Approach for Time-dependent Reliability of Dynamic Systems with Random Parameters Excited by Input Random Processes

Igor Baseski^{1,2}, Dorin Drignei³, Zissimos P. Mourelatos¹, Monica Majcher¹
Oakland University, Rochester MI 48309

¹Mechanical Engineering Department, ²U.S. Army TARDEC, Warren MI 48397, ³Math & Statistics Department

Copyright © 2014 SAE International

Abstract

We propose a new metamodeling method to characterize the output (response) random process of a dynamic system with random parameters, excited by input random processes. The metamodel can be then used to efficiently estimate the time-dependent reliability of a dynamic system using analytical or simulation-based methods. The metamodel is constructed by decomposing the input random processes using principal components or wavelets and then using a few simulations to estimate the distributions of the decomposition coefficients. A similar decomposition is also performed on the output random process. A kriging model is then established between the input and output decomposition coefficients and subsequently used to quantify the output random process corresponding to a realization of the input random parameters and random processes. What distinguishes our approach from others in metamodeling is that the system input is not deterministic but random. The quantified output random process is finally used to estimate the time-dependent reliability or probability of failure of the dynamic system using the total probability theorem. The proposed method is illustrated with a numerical example.

1. Introduction

The response of dynamic systems under uncertainty is described by a random process. The input commonly consists of a combination of random variables and random processes. A time-dependent reliability analysis is therefore, needed to calculate the probability that the system will perform its intended function successfully for a specified time. It is therefore, related to product functionality over time.

Reliability is an important engineering requirement for consistently delivering acceptable product performance through time. As time progresses, the product may fail due to time-dependent operating conditions and material properties, component degradation, etc. In this research, we use time-dependent reliability concepts associated with the first-passage of non-repairable systems.

The time-dependent probability of failure, or cumulative probability of failure [1, 2], is defined as

$$P_f(0,T) = P\{\exists t \in [0,T] : g(\boldsymbol{\beta}, \mathbf{Z}(t), t) \ge S_t \}$$
(1)

where g is a random process that maps the input random variables $\mathbf{\beta}$ and random processes $\mathbf{Z}(t)$ to a response of interest and S_t is a given threshold value. The random process $G(t) = g(\mathbf{\beta}, \mathbf{Z}(t), t) - S_t$ can be viewed as a collection of random variables at different time instances t. Since we consider a first excursion failure problem in Equation (1), the failure domain is defined as $F = \left\{ \max_{t \in [0,T]} g(\mathbf{\beta}, \mathbf{Z}(t), t) \geq S_t \right\}$.

The time-dependent probability of failure of Equation (1) can be calculated exactly as

$$P_{\mathbf{f}}\left(0,T\right) = 1 - (1 - P_{\mathbf{f}}^{\mathbf{i}}\left(0\right)) \exp\left\{-\int_{0}^{T} \lambda\left(t\right) dt\right\}$$
 (2)

where $\mathit{P}_{f}^{i}\left(0\right)$ is the instantaneous probability of failure at the

initial time and
$$\lambda(t) = \lim_{dt \to 0} \frac{P(t < T_f \le t + dt \mid T_f > t)}{dt}$$
 is the

failure rate with $T_{
m f}$ denoting the time to failure. In the commonly used out-crossing rate approach, the failure rate is approximated by the up-crossing rate

$$v^{+}(t) = \lim_{\Delta \tau \to 0} \frac{P \left[g(\boldsymbol{\beta}, \mathbf{Z}(t), t) - S_{t} < 0 \cap g(\boldsymbol{\beta}, \mathbf{Z}(t + \Delta \tau), t + \Delta \tau) - S_{t} \ge 0 \right]}{\Delta \tau}$$
$$\Delta \tau > 0$$

(3)

under the assumptions that the probability of having two or more out-crossings in $[t, t + \Delta t]$ is negligible, and the out-crossings in $[t, t + \Delta t]$ are statistically independent of the previous out-crossings in [0, t].

Monte Carlo simulation (MCS) can accurately estimate the probability of failure in Equation (1) but it is computationally prohibitive for dynamic systems with a low failure probability. To

Report Documentation Page

Form Approved OMB No. 0704-0188

Public reporting burden for the collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to a penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number.

1. REPORT DATE 09 APR 2014	2. REPORT TYPE Journal Article	3. DATES COVERED 08-02-2014 to 15-03-2014	
4. TITLE AND SUBTITLE A New Metamodeling Approach for Time-dependent Reliability of Dynamic Systems with Random Parameters Excited by Input Random Processes		5a. CONTRACT NUMBER W56HZV-04-2-0001	
		5b. GRANT NUMBER	
		5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)	5d. PROJECT NUMBER		
Igor Baseski; Dorin Drignei; Zissimo	5e. TASK NUMBER		
		5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND A Oakland University,2200 N. Squirrel	8. PERFORMING ORGANIZATION REPORT NUMBER ; #24310		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSOR/MONITOR'S ACRONYM(S)	
U.S. Army TARDEC, 6501 East Eleven Mile Rd, Warren, Mi,		TARDEC	
48397-5000		11. SPONSOR/MONITOR'S REPORT NUMBER(S) #24310	

12. DISTRIBUTION/AVAILABILITY STATEMENT

Approved for public release; distribution unlimited

13. SUPPLEMENTARY NOTES

Submitted to SAE World Congress 2014

14. ABSTRACT

We propose a new metamodeling method to characterize the output (response) random process of a dynamic system with random parameters, excited by input random processes. The metamodel can be then used to efficiently estimate the time-dependent reliability of a dynamic system using analytical or simulation-based methods. The metamodel is constructed by decomposing the input random processes using principal components or wavelets and then using a few simulations to estimate the distributions of the decomposition coefficients. A similar decomposition is also performed on the output random process. A kriging model is then established between the input and output decomposition coefficients and subsequently used to quantify the output random process corresponding to a realization of the input random parameters and random processes. What distinguishes our approach from others in metamodeling is that the system input is not deterministic but random. The quantified output random process is finally used to estimate the time-dependent reliability or probability of failure of the dynamic system using the total probability theorem. The proposed method is illustrated with a numerical example.

a. REPORT unclassified	b. ABSTRACT unclassified	c. THIS PAGE unclassified	Public Release	OF PAGES 7	RESPONSIBLE PERSON		
16. SECURITY CLASSIFICATION OF:			17. LIMITATION	18. NUMBER	19a. NAME OF		
15. SUBJECT TERMS							

address the computational issue of MCS, analytical methods have been developed based on the out-crossing rate approach which was first introduced by Rice [3] followed by extensive studies [2, 4-6] under the assumption that the out-crossings are statistically independent and Poisson distributed. The PHI2 method [2] uses two successive time-invariant analyses based on FORM, and the binomial cumulative distribution to calculate the probability of the joint event in Equation (3). A Monte-Carlo based set theory approach has been also proposed [7, 8] using a similar approach with the PHI2 method. Because, analytical studies (e.g., [9-11]) have shown that the PHI2 based approach lacks sufficient accuracy for vibratory systems, analytical approaches have been proposed to accurately estimate the time-dependent probability of failure considering non-monotonic behavior [9, 12, 13].

The limited accuracy of the out-crossing rate approach has been recently improved by considering the correlations between the limit-state function at two time instants [11]. The method estimates the up-crossing rate $v^+(t)$ by solving an integral equation involving $v^+(t)$ and $v^{++}(t,t_1)$, the joint probability of up-crossings in times t and t_1 [14].

Among the simulation-based methods, a MCS approach was proposed in [15] to estimate the time-dependent failure rate over the product lifecycle and its efficiency was improved using an importance sampling method with a decorrelation length [16] in order to reduce the high dimensionality of the problem. Subset simulation [17, 18] has been recently developed as an efficient simulation method for computing small failure probabilities for general reliability problems. Its efficiency comes from introducing appropriate intermediate failure sub-domains to express the low probability of failure as a product of larger conditional failure probabilities which are estimated with much less computational effort. Because it is very challenging to generate samples in the conditional spaces, subset simulation with Markov Chain Monte Carlo (SS/MCMC) [19] and subset simulation with splitting (SS/S) [20, 21] methods have been introduced.

In this paper, we describe a new metamodeling method to characterize the output random process of a dynamic system with random parameters, excited by input random processes which can be used to efficiently estimate the time-dependent probability of failure using either analytical or simulation-based methods. The metamodel is constructed by decomposing the input random processes using principal components or wavelets and then using a few simulations to estimate the distributions of the decomposition coefficients. A similar decomposition is also performed on the output random process. A kriging model is then established between the input and output decomposition coefficients and subsequently used to quantify the output random process corresponding to a realization of the input random parameters and random processes. The proposed approach is new because it considers the system input as random and not deterministic as is usually the case.

The paper is arranged as follows. Section 2 describes the proposed metamodeling methodology and Section 3 uses a mathematical example to demonstrate its applicability. Finally, Section 4 provides a brief summary and concludes.

2. PROPOSED METAMODELING APPROACH

Assume that the simulation model has two types of inputs: random time-dependent inputs represented by the random $\mathbf{Z}(t)$ and random time-independent processes represented by random variables **β**. Assume that the output is also time-dependent and is represented by the random processes Y(t). We decompose each process Z(t) using a well-defined basis of functions $\mathbf{B}(t)$ such as wavelets or principal components. For principal components, consider D realizations of the random process Z(t) denoted $Z_1(t)$..., $Z_D(t)$. An eigenvalue decomposition of their covariance matrix defines the principal components. If we retain a small number r of dominant eigenvalues and $\mathbf{B_1}(t)$ is a vector whose rows are the corresponding eigenvectors, each $Z_{i}(t), j = 1, ..., D$ can be expressed $Z_{j}(t) = \sum_{i=1}^{r} \alpha_{i} B_{1i}(t) = \alpha_{j} \mathbf{B_{1}}(t) \text{ where } \alpha_{j} = Z_{j}(t) \mathbf{B_{1}}(t)^{T}.$ Α similar principal decomposition can be considered for the output process Y(t) so that each output realization (sample $Y_i(t), j = 1, \ldots, D$ can be expressed $Y_j(t) = \sum_{i=1}^{S} \delta_i B_{2i}(t) = \delta_j \mathbf{B_2}(t)$ using basis functions $\mathbf{B_2}(t)$ and $\delta_i = Y_i(t) \mathbf{B_2}(t)^T$, if we retain a small number s of dominant eigenvalues of the output covariance matrix.

To simplify the description of the proposed method, we assume that we have only one input random variable $\beta,$ one input random process Z(t), and one output random process Y(t) which is represented with only one principal component. The input vector can be therefore, expressed in terms of the vector $(\mathbf{\alpha},\ \beta)$ where $\mathbf{\alpha}=\left(\alpha_1,\alpha_2,...,\alpha_r\right)$ and the output is expressed in terms of δ_1 . We use the principal component decomposition in this paper although other bases may be chosen (e.g. wavelets).

What distinguishes our approach from others in metamodeling is that the input vector (α, β) is not deterministic but random. The distributions of all components of (α, β) are estimated using a small number of computer runs. If we assume that all α_i 's are independent and normally distributed as $N(\mu_i, \sigma_i^2)$ where μ_i is the mean of α_i over all performed computer runs and σ_i is the standard error of α_i over all computer runs, and also assume that β is a normal random variable with mean μ_β and standard error σ_β , independent of the α 's, the joint probability density function between α and β is given by

$$f(\boldsymbol{\alpha}, \boldsymbol{\beta}) = \frac{1}{\left(\sqrt{2\pi}\right)^r \sigma_1 \dots \sigma_r} \exp\left[-\frac{1}{2} \sum_{i=1}^r \frac{\left(\alpha_i - \mu_i\right)^2}{\sigma_i^2}\right].$$

$$\cdot \frac{1}{\sigma_{\boldsymbol{\beta}} \sqrt{2\pi}} \exp\left[-\frac{1}{2} \frac{\left(\boldsymbol{\beta} - \mu_{\boldsymbol{\beta}}\right)^2}{\sigma_{\boldsymbol{\beta}}^2}\right] \tag{4}$$

We run the mathematical model for D input vectors $(\boldsymbol{\alpha}^{(1)}, \boldsymbol{\beta}^{(1)}), \ldots, (\boldsymbol{\alpha}^{(D)}, \boldsymbol{\beta}^{(D)})$ and obtain the corresponding time-dependent outputs whose first principal component is $(\boldsymbol{\delta}^{(1)}, \ldots, \boldsymbol{\delta}^{(D)})$. Denote the vectors $\underline{\boldsymbol{\alpha}} = (\boldsymbol{\alpha}^{(1)}, \ldots, \boldsymbol{\alpha}^{(D)}), \underline{\boldsymbol{\beta}} = (\boldsymbol{\beta}^{(1)}, \ldots, \boldsymbol{\beta}^{(D)})$ and $\underline{\boldsymbol{\delta}} = (\boldsymbol{\delta}^{(1)}, \ldots, \boldsymbol{\delta}^{(D)})$. Conditioned on $(\underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}})$, the vector $\underline{\boldsymbol{\delta}}$ has a multivariate Gaussian distribution with mean η 1 and

covariance matrix $\tau^2 C$ where C is a Gaussian correlation matrix whose elements depend on the distances between sampled inputs (α, β) . The parameters of this distribution are estimated by maximum likelihood.

Let $\left(\alpha_0,\beta_0\right)$ be a new input vector and δ_0 the corresponding output first principal component. A kriging metamodel is generated between the input $\left(\underline{\alpha},\,\underline{\beta}\right)$ and the output $\underline{\delta}$ to obtain δ_0 . Details about kriging metamodeling can be found, for example, in [22-24]. The kriging Gaussian prediction distribution $\hat{f}(\delta_0 \mid \underline{\alpha}, \underline{\beta})$ for δ_0 , is given by

$$\hat{f}(\delta_0 \mid \underline{\alpha}, \underline{\beta}) = \frac{1}{\sqrt{2\pi v_{\underline{\alpha}, \underline{\beta}}^0}} \exp \left[-\frac{1}{2v_{\underline{\alpha}, \underline{\beta}}^0} \left(\delta_0 - m_{\underline{\alpha}, \underline{\beta}}^0 \right)^2 \right]$$
 (5)

where the prediction variance is $v_{\underline{\alpha},\underline{\beta}}^0 = \tau^2 \Big(1 - \mathbf{C}_0^T \mathbf{C}^{-1} \mathbf{C}_0 \Big)$ and the prediction mean is $m_{\underline{\alpha},\underline{\beta}}^0 = \eta + \mathbf{C}_0^T \mathbf{C}^{-1} \Big(\underline{\delta} - \eta \mathbf{1} \Big)$. Here \mathbf{C}_0 is the vector of correlations between the new input and the sampled inputs. The joint distribution of $\delta_0,\underline{\alpha},\beta$ is

$$\hat{f}(\delta_{0}, \underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}}) = \hat{f}(\delta_{0} | \underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}}) f(\underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}}) \propto
\frac{1}{\sqrt{2\pi\nu} \underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}}} \exp \left[-\frac{1}{2\nu \underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}}} \left(\delta_{0} - m_{\underline{\boldsymbol{\alpha}}, \underline{\boldsymbol{\beta}}}^{0} \right)^{2} \right]
D = \sum_{j=1}^{D} \exp \left[-\frac{1}{2} \sum_{i=1}^{r} \frac{(\alpha_{i}^{(j)} - \mu_{i})^{2}}{\sigma_{i}^{2}} - \frac{1}{2} \frac{(\beta^{(j)} - \mu_{\beta})^{2}}{\sigma_{\beta}^{2}} \right] (6)$$

The marginal distribution of $\,\delta_0\,$ at the new input vector $\left(a_0,\beta_0\right)$ is given by the integral

$$\hat{f}(\delta_0) = \int \hat{f}(\delta_0, \underline{\alpha}, \beta) \, d\underline{\alpha} \, d\beta. \tag{7}$$

Note that the typically small number of runs performed in an engineering problem is used only to estimate the distributions $f(\underline{\alpha},\underline{\beta})$ and $\hat{f}(\delta_0 \mid \underline{\alpha},\underline{\beta})$ of Equations (4) and (5), respectively. Once these distributions are estimated, a larger number N of statistical simulations from the distribution $\hat{f}(\delta_0)$ of Equation (7) can be obtained. For each simulated δ_0 we create a simulated output function $\hat{Y}_0(t) = \delta_0 B_2(t)$.

We now provide some details on the evaluation of integral in Equation (7). Consider R sampled sets of D input vectors $(\underline{\alpha},\underline{\beta})_1,...,(\underline{\alpha},\underline{\beta})_R$. The integral is approximated using the Monte Carlo method, up to a proportionality constant, as

$$\frac{1}{R} \sum_{k=1}^{R} \hat{f}(\delta_0, (\underline{\alpha}, \underline{\beta})_k) = \frac{1}{R} \sum_{k=1}^{R} \hat{f}(\delta_0 \mid (\underline{\alpha}, \underline{\beta})_k) f((\underline{\alpha}, \underline{\beta})_k). \tag{8}$$

While $f((\underline{\alpha},\underline{\beta})_k)$ can be computed easily for any number R of sets, $\hat{f}(\delta_0 \mid (\underline{\alpha},\underline{\beta})_k)$ will require running the mathematical model R^*D times; i.e., for each set $[(\underline{\alpha},\underline{\beta})_k,\gamma]$ of D input vectors. This is computationally very demanding. Instead, we use a jackknife method (e.g. [25]), which belongs to the general class of "leave-one-out" methods for cross-validation. Specifically, we choose R=D and $(\underline{\alpha},\underline{\beta})_k:=(\underline{\alpha}^{(-k)},\underline{\beta}^{(-k)})$, meaning that we replace $(\underline{\alpha},\underline{\beta})_k$ by the set of D original input vectors $\underline{\alpha},\underline{\beta}$ from which we leave the k^{th} input vector out, for k=1,...,D. The advantage of this method is that we already have data from math model runs at these $(\underline{\alpha}^{(-k)},\underline{\beta}^{(-k)})$ vectors, and we do not need any additional math model runs.

The total probability theorem is used to compute the time-dependent probability of failure. We draw M new random inputs $\left(a_0,\beta_0\right)$ from the input distribution $f\left(a,\beta\right)$ of Equation (4) and for each of them simulate N output random functions $\hat{Y}_0(t)$ by sampling $\hat{f}\left(\delta_0\right)$ of Equation (7) N times. For each of the M random inputs $\left(a_0,\beta_0\right)$, a simple Monte Carlo simulation is used to calculate a probability of failure $P_f^M\left(0,t\right)$ using the N output functions $\hat{Y}_0(t)$. It can be easily shown using the total probability theorem that the probability of failure is the average among the $P_f^M\left(0,t\right)$ probabilities; i.e.,

 $P_f\left(0,t\right) = rac{1}{M} \sum_{i=1}^M P_f^M\left(0,t\right)$. Therefore, the time-dependent probability of failure is the percentage of the M^*N response functions $\hat{Y}_0(t)$ that exceed a specified failure threshold T in the interval [0,t]. This probability considers the randomness of the inputs Z(t) and β .

3. EXAMPLE

Consider the following mathematical model

$$Y(t) = 2\exp(Z(t))\sin(2\pi\beta t)$$
(9)

where Z(t) is a random process generated from the function 2-t, to which correlated noise has been added. The correlated noise is represented by random draws from a Gaussian distribution with a zero mean vector and Gaussian correlation

for the temporal dimension of smoothness parameter 25. The random parameter β is normally distributed as N(2, 0.05).

A sample of D=30 computer runs is obtained (Figure 1). Figure 1a shows the sample of 30 random input functions Z(t) for $t\in [0,\,2]$ and Figure 1b shows their principal component reconstruction using r=4 principal components which account for approximately 90% of the variance. Figure 1c shows the corresponding 30 random output functions Y(t) and Figure 1d shows their principal component reconstruction using only the first principal component which accounts for about 66% of the variability. Visual inspection shows that the time-dependent output reconstruction captures the major features of actual time-dependent output, even with only the first principal component.

The random input vector is expressed with 5 components: the 4 coefficients from the principal component decomposition of the input function Z(t) denoted by α and the β . The time-dependent output is expressed by a scalar which is the dominant principal component coefficient δ . The four components of α are assumed independent and normal, with estimated means equal to zero and standard deviations equal to 0.9062, 0.8387, 0.6854, and 0.4947, respectively. These estimated values are obtained from the sample of 30 computer runs. The estimated mean and standard deviation of β are 1.9997 and 0.0531 respectively, which are in agreement with the theoretical values of 2 and 0.05. The scatter plots of Figure 2 verify the assumption that the four components of α are independent.

We have developed a metamodel using the proposed approach using M = 100 new random inputs drawn from the input distribution and N = 50 simulations for each of these new random inputs. Therefore, we have a total of 5,000 simulations $Y_0(t)$ shown in green in the left panel of Figure 3. We observe that the variability of these curves appears to be similar with the variability of the 30 actual math model output curves (Figure 1c) or their principal components reconstructions (Figure 1d). However, their number is 5,000 (much greater than 30), which allows for a more accurate evaluation of the probability of failure. The right panel of Figure 3 shows the time-dependent probability of exceeding the thresholds T of 4, 6, 7.5, 10 or 15. We observe as expected, that as the threshold is increased the time-dependent probability of failure reaches its maximum value of 1 at a later time. The accuracy of the calculated probabilities of failure can be easily verified using Monte Carlo simulation.

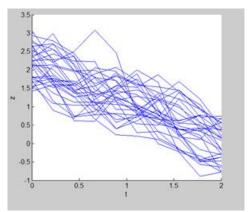
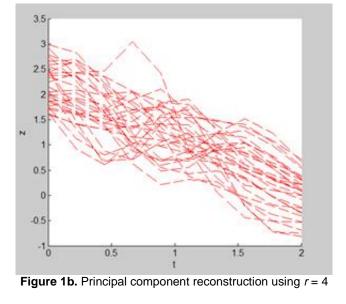


Figure 1a. A sample of 30 random input functions Z(t)



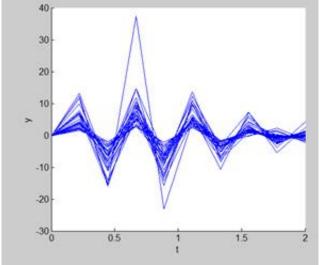


Figure 1c. Corresponding 30 random output functions Y(t)

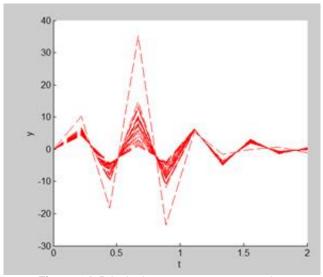


Figure 1d. Principal component reconstruction

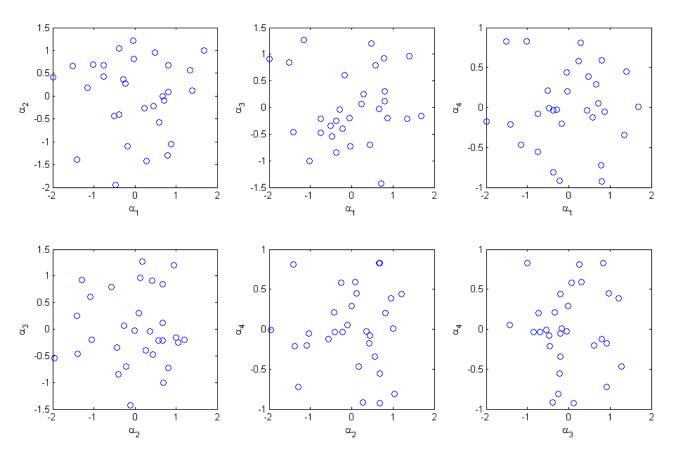


Figure 2. Scatter plots of the four components of vector $\boldsymbol{\alpha}$

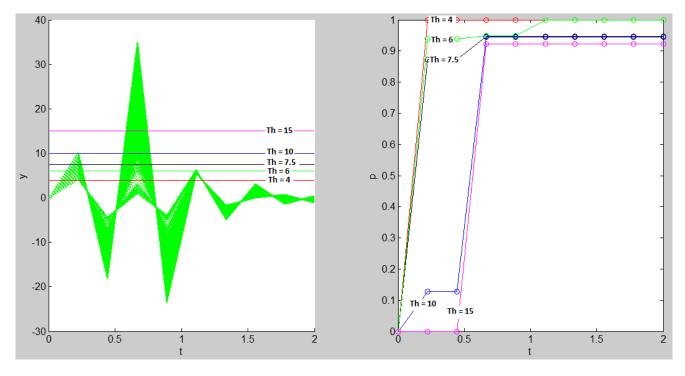


Figure 3. Metamodel simulations (left panel) and time-dependent probability for different thresholds (right panel)

4. Summary/Conclusions

We described in this paper a new metamodeling approach to characterize the output random process of a dynamic (or time-dependent in general) system with random input parameters, excited by an input random process. The methodology utilizes a decomposition of the input and output random processes using principal components or wavelets and kriging. The latter establishes a non-parametric interpolation between the input and output decomposition coefficients which is then used to quantify the output random process. The metamodel is used to efficiently estimate the time-dependent probability of failure using either analytical or simulation-based methods. This capability is very practical and desirable for large-scale, linear or non-linear, dynamic systems where the calculation of response is time intensive and/or expensive to compute or measure. The proposed approach considers the system input as random and not deterministic as is usually the case. We used a simple mathematical example to demonstrate the steps of the approach and demonstrate its practicality. Future work will generalize the method for non-Gaussian random variables and processes.

Acknowledgments

We would like to acknowledge the technical and financial support of the Automotive Research Center (ARC) in accordance with Cooperative Agreement W56HZV-04-2-0001 U.S. Army Tank Automotive Research, Development and Engineering Center (TARDEC) Warren, MI.

References

- Singh, A., Mourelatos, Z. P., and Li, J., 2010, "Design for Lifecycle Cost using Time-dependent Reliability," ASME Journal of Mechanical Design, 132(9), 091008 (11 pages).
- Andrieu-Renaud, C., Sudret, B., and Lemaire, M., 2004, "The PHI2 Method: A Way to Compute Time-Variant Reliability", Reliability Engineering and Safety System, 84(1), 75-86.
- Rice, S. O., 1954, "Mathematical Analysis of Random Noise," *Bell Syst Tech J*, 23, 282–332. [Re-published in: Wax N, editor. *Selected Papers on Noise and Stochastic Processes*, New York, Dover, 1954].
- Rackwitz, R., 1998, "Computational Techniques in Stationary and Non-Stationary Load Combination – A Review and Some Extensions," *Journal of Structural Engineering*, 25(1), 1-20.
- 5. Sudret, B., 2008, "Analytical Derivation of the Outcrossing Rate in Time-variant Reliability Problems," *Structure and Infrastructure Engineering*, 4(5), 356-362.
- Zhang, J., and Du, X., 2011, "Time-dependent Reliability Analysis for Function Generator Mechanisms," ASME Journal of Mechanical Design, 133(3), 031005 (9 pages).
- Savage, G. J., and Son, Y. K., 2009, "Dependability-Based Design Optimization of Degrading Engineering Systems," ASME Journal of Mechanical Design, 131(1), 011002 (10 pages).
- Son, Y. K., and Savage, G. J., 2007, "Set Theoretic Formulation of Performance Reliability of Multiple Response Time-Variant Systems due to Degradations in System Components," Quality and Reliability Engineering International, 23(2), 171-188.

- 9. Singh, A., and Mourelatos, Z. P., 2010, "On the Time-dependent Reliability of Non-Monotonic, Non-Repairable Systems," SAE International Journal of Materials and Manufacturing, 3(1), 425-444.
- Hu, Z., and Du, X., 2012, "Time-dependent Reliability Analysis by a Sampling Approach to Extreme Values of Stochastic Processes," Proceedings of ASME 2012 Design Engineering Technical Conferences, Paper DETC2012-70132, Chicago, IL.
- Hu, Z., Li, H., Du, X., and Chandrashekhara, K., 2012, "Simulation-based Time-dependent Reliability Analysis for Composite Hydrokinetic Turbine Blades," *Structural and Multidisciplinary Optimization*, DOI 10.1007/s00158-012-0839-8.
- Li, J., and Mourelatos, Z. P., 2009, "Time-Dependent Reliability Estimation for Dynamic Problems using a Niching Genetic Algorithm," ASME Journal of Mechanical Design, 131(7).
- Hu, Z., and Du, X., 2012, "Reliability Analysis for Hydrokinetic Turbine Blades," Renewable Energy, 48, 251-262.
- 14. Madsen, P. H., and Krenk, S., 1984, "An Integral Equation Method for the First Passage Problem in Random Vibration," *Journal of Applied Mechanics*, 51, 674-679.
- Singh, A., and Mourelatos, Z. P., 2010, "Time-Dependent Reliability Estimation for Dynamic Systems Using a Random Process Approach," SAE International Journal of Materials & Manufacturing, 3(1), 339-355.
- Singh, A., Mourelatos, Z. P., and Nikolaidis, E., 2011, "Time-Dependent Reliability of Random Dynamic Systems using Time-Series Modeling and Importance Sampling," SAE International Journal of Materials & Manufacturing, 4(1), 929-946.
- Au, S. K., and Beck, J. L., 2001, "Estimation of Small Failure Probability in High Dimensions Simulation," Probabilistic Engineering Mechanics, 16, 263-277.
- Au, S. K., and Beck, J. L., 2003, "Subset Simulation and its Application to Seismic Risk Based on Dynamic Analysis," *Journal of Engineering Mechanics*, 129, 901-917.
- Beck, J. L., and Au, S. K., 2002, "Bayesian Updating of Structural Models and Reliability Using Markov Chain Monte Carlo Simulation," *Journal of Engineering Mechanics*, 128(4), 380-391.
- Ching, J., Beck, J. L., and Au, S. K., 2005, "Reliability Estimation for Dynamic Systems Subject to Stochastic Excitation Using Subset Simulation with Splitting," Computer Methods in Applied Mechanics and Engineering, 194, 1557-1579.
- Wang, Z., Mourelatos, Z. P., Li, J., Singh, A., and Baseski, I., 2013, "Time-dependent Reliability of Dynamic Systems using Subset Simulation with Splitting over a Series of Correlated Time Intervals," *Proceedings of ASME 2013* Design Engineering Technical Conferences, Paper DETC2013-12257, Portland, OR.
- Currin, C., Mitchell, T., Morris, M., and Ylvisaker D., 1991, "Bayesian Prediction of Deterministic Functions, with Applications to the Design and Analysis of Computer Experiments," *Journal of the American Statistical* Association, 86, 953-963.
- Sacks, J., Welch, W. J., Mitchell, T. J., and Wynn, H. P., 1989, "Design and Analysis of Computer Experiments," Statistical Science, 4, 409-423.
- 24. Santner, T. J., Williams, B. J., and Notz, W. I., 2003, *The Design and Analysis of Computer Experiments*, Springer.

25. Rizzo, M. L., 2007, *Statistical Computing with R*, Chapman and Hall.

Contact Information

Zissimos P. Mourelatos, Ph.D. Mechanical Engineering Department Oakland University Rochester, MI 48309 Tel: 248-370-2686 mourelat@oakland.edu